

An Optical Study on the Coagulation and Peptization of Silver Iodide Colloidal Solutions by Surface Active Agent

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Introduction

The study on the phenomena of coagulation and peptization of colloidal or macromolecular solutions by surface active agents initiated by Tamamushi⁽¹⁾ in 1947 has been developed by a number of investigators in this country. ⁽²⁾⁽³⁾⁽⁴⁾

The author has studied, under the guidance of Prof. B. Tamamushi, the effect of a cationic surface active agent, dodecylamine hydrochloride,* on the coagulation and peptization of the colloidal solution of silver iodide, the particle of which was negatively charged. When a small amount of D. A. H. is added to the solution, it becomes turbid due to the coagulation of the colloid particles, and the turbidity increases with the concentration of D. A. H. added. But at a certain concentration of D. A. H., the effect of the agent reverses from coagulation to peptization and the turbidity begins to decrease with the rise of the concentration of D. A. H., the peptized AgI sol being charged positively. The change of the percentage transmittance of the mixed solution with the concentration of D. A. H. is shown in Fig. 1.

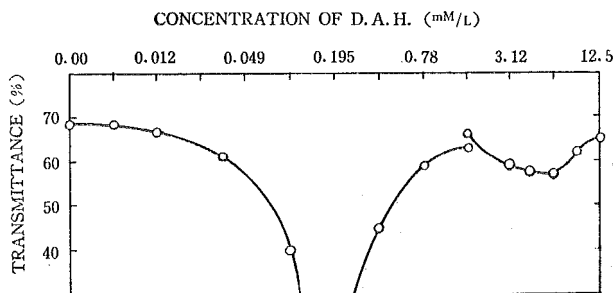


Fig. 1. Percentage transmittance of AgI sol of 2.2mM/L, obtained 20 minutes after D. A. H. of varied concentrations was added. Wavelength of photometer is 650m μ . Coagulation value is 0.08mM/L.

* Henceforce to be abbreviated as D. A. H.

The main object of this study is to examine the change of the state of the colloidal solution in the course of coagulation and peptization processes, especially to detect the difference of state of sols just before coagulation and after peptization by applying the optical methods, namely, the transmittance measurement on one hand and the particle size measurement on the other.

Experimental

160 cc of 0.01M/L silver nitrate solution is added to 200 cc of 0.01 M/L potassium iodide solution, the mixing being carried out quickly and thoroughly. The silver iodide sol thus prepared has the concentration of 4.4 mM/L (as AgI) and is charged negatively.

The sol is then purified by electrodialysis. As the sol is sensitive to light, it should be kept from light during this procedure. The percentage of transmittance obtained with the purified sol and its dilutions is shown in Table 1. A good linearity holds between the concentration and the logarithm of transmittance, which proves the Rule of Lambert-Beer.

Table 1. Percentage transmittance of AgI sol of various concentrations.

| CONC. $\lambda_0(m\mu)$ | 4.4 (mM/L) | 2.2 " | 1.1 " |
|----------------------------|------------|-------|-------|
| 450 | 2.2% | 13.2% | 36.2% |
| 500 | 13.0 | 36.0 | 59.6 |
| 550 | 29.0 | 53.1 | 72.6 |
| 600 | 43.1 | 65.1 | 80.2 |
| 650 | 56.0 | 74.2 | 86.0 |
| 700 | 66.1 | 81.0 | 90.0 |
| 750 | 73.4 | 85.2 | 92.0 |
| 800 | 79.0 | 88.8 | 94.0 |
| 850 | 83.1 | 91.0 | 95.0 |
| 900 | 86.9 | 93.0 | 96.2 |
| 950 | 89.1 | 94.0 | 97.0 |
| 1000 | 91.1 | 95.2 | 97.1 |
| 1040 | 92.5 | 96.1 | 97.8 |
| 1080 | 93.2 | 96.5 | 98.0 |
| 1100 | 93.5 | 96.8 | 98.0 |
| 1120 | 93.5 | 96.5 | 98.0 |
| 1160 | 93.0 | 96.2 | 98.0 |
| 1200 | 92.0 | 95.8 | 97.4 |

(λ_0 : wavelength in air)

Table 2 and Figures 2~3 show the transmittance percentage of the mixed solutions of the silver iodide sol and D. A. H. solution of the same volume

but various concentrations, where "t" denotes the time between the mixing and the observation and λ_0 the wavelength of light in air.

When the concentration of D. A. H. is below 0.035 mM/L , the transmittance percentage immediately after the mixing is the same with that of the original sol of 2.2 mM/L concentration. But when the sol is mixed with D. A. H. whose concentrations are greater than 0.39 mM/L in the mixed solutions, some increase of turbidity can be observed at once. Such increase of turbidity is most remarkable when the D. A. H. concentration is 0.39 mM/L as shown in Table 2 and Fig. 2.

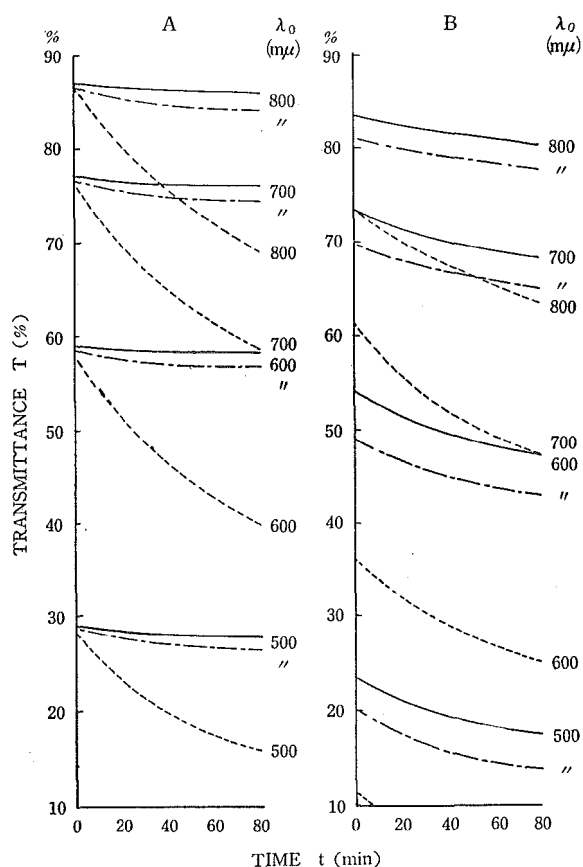


Fig. 2. Change of transmittance after the mixing.

| | CONC. of D. A. H. | |
|--------|----------------------|---------------------|
| | A | B |
| solid | 0.006 mM/L | 1.56 mM/L |
| chain | 0.012 mM/L | 0.78 mM/L |
| dotted | 0.035 mM/L | 0.39 mM/L |

Table 2a. Percentage transmittance of the mixed solutions.

| D. A. H. CONC. λ_0 (m μ) | 0.006 (mM/L) | 0.012 " | 0.035 " | t (min.) |
|--|--------------|---------|---------|----------|
| | % | % | % | |
| 450 | 8.9 | 8.7 | 7.5 | 5 |
| 500 | 28.9 | 28.3 | 25.8 | 6 |
| 550 | 45.6 | 45.0 | 42.0 | 7 |
| 600 | 59.0 | 58.2 | 55.0 | 8 |
| 650 | 69.2 | 68.4 | 64.9 | 9 |
| 700 | 76.5 | 75.8 | 72.0 | 10 |
| " * | 76.8 | 76.0 | 72.7 | 11 |
| 750 | 82.5 | 81.7 | 78.2 | 12 |
| 800 | 86.4 | 85.7 | 82.3 | 13 |
| 850 | 89.0 | 88.2 | 85.0 | 14 |
| 900 | 91.2 | 90.5 | 87.7 | 15 |
| 950 | 92.9 | 92.0 | 89.2 | 16 |
| 1000 | 94.2 | 93.3 | 91.0 | 17 |
| 1050 | 95.0 | 94.5 | 92.0 | 18 |
| 1080 | 95.0 | 94.5 | 92.0 | 19 |
| 1100 | 95.2 | 94.8 | 92.0 | 20 |
| 1150 | 95.2 | 94.7 | 92.0 | 21 |
| 1200 | 94.9 | 94.1 | 91.4 | 22 |
| 450 | 8.8 | 8.5 | 6.2 | 23 |
| 500 | 28.5 | 28.0 | 22.1 | 24 |
| 550 | 45.7 | 44.7 | 37.6 | 25 |
| 600 | 58.5 | 57.2 | 49.7 | 26 |
| 650 | 69.0 | 68.2 | 59.6 | 27 |
| 700 | 76.3 | 75.2 | 68.0 | 28 |
| " * | 76.8 | 75.3 | 68.0 | 29 |
| 750 | 82.0 | 81.0 | 73.9 | 30 |
| 800 | 86.0 | 84.9 | 77.8 | 31 |
| 850 | 88.9 | 87.5 | 81.0 | 32 |
| 900 | 91.0 | 90.0 | 83.6 | 33 |
| 950 | 93.0 | 92.0 | 86.0 | 34 |
| 1000 | 94.0 | 93.0 | 88.0 | 35 |
| 1050 | 95.0 | 94.6 | 89.4 | 36 |
| 1080 | 95.1 | 94.2 | 89.2 | 37 |
| 1100 | 95.0 | 94.7 | 89.5 | 38 |
| 1150 | 95.0 | 94.5 | 89.0 | 39 |
| 1200 | 95.0 | 94.0 | 88.5 | 40 |
| 450 | 8.5 | 8.0 | 5.0 | 41 |
| 500 | 28.0 | 27.0 | 18.8 | 42 |
| 550 | 45.0 | 43.8 | 33.0 | 43 |
| 600 | 58.7 | 57.0 | 45.0 | 44 |
| 650 | 69.0 | 67.2 | 55.0 | 45 |
| 700 | 76.0 | 74.7 | 63.2 | 46 |
| " * | 76.5 | 75.0 | 63.8 | 47 |
| 750 | 82.0 | 80.5 | 69.8 | 48 |
| 800 | 86.0 | 84.5 | 73.8 | 49 |
| 850 | 88.7 | 87.2 | 77.0 | 50 |
| 900 | 91.0 | 89.9 | 80.0 | 51 |
| 950 | 92.5 | 91.5 | 82.5 | 52 |
| 1000 | 94.0 | 93.1 | 85.0 | 53 |
| 1050 | 95.0 | 94.0 | 86.0 | 54 |

| D. A. H. CONC. λ_0 (m μ) | 0.39 (mM/L) | 0.78 " | 1.56 " | t (min.) |
|--|-------------|--------|--------|----------|
| | % | % | % | |
| 450 | 1.4 | 4.0 | 5.0 | 11 |
| 500 | 9.0 | 18.2 | 22.0 | 12 |
| 550 | 20.2 | 34.0 | 38.4 | 13 |
| 600 | 33.0 | 47.5 | 52.0 | 14 |
| 650 | 45.1 | 59.3 | 63.2 | 15 |
| 700 | 55.2 | 68.2 | 71.8 | 16 |
| " * | 55.3 | 68.6 | 71.8 | 18 |
| 750 | 64.6 | 75.0 | 78.0 | 19 |
| 800 | 70.0 | 80.0 | 82.5 | 20 |
| 850 | 75.0 | 83.9 | 86.0 | 21 |
| 900 | 79.0 | 87.0 | 88.9 | 22 |
| 950 | 82.7 | 89.3 | 91.0 | 23 |
| 1000 | 86.0 | 91.6 | 92.9 | 25 |
| 1050 | 88.0 | 92.8 | 94.0 | 26 |
| 1080 | 88.5 | 93.1 | 94.1 | 27 |
| 1100 | 88.3 | 93.0 | 94.0 | 28 |
| 1150 | 88.0 | 92.8 | 93.9 | 29 |
| 1200 | 87.0 | 92.1 | 93.1 | 30 |
| 450 | 1.0 | 3.2 | 4.8 | 32 |
| 500 | 6.8 | 16.2 | 20.0 | 33 |
| 550 | 17.0 | 31.8 | 36.1 | 34 |
| 600 | 29.1 | 45.5 | 50.0 | 35 |
| 650 | 41.1 | 57.5 | 61.5 | 36 |
| 700 | 51.3 | 66.8 | 70.0 | 38 |
| " * | 52.2 | 67.2 | 70.5 | 40 |
| 750 | 60.3 | 73.9 | 76.9 | 41 |
| 800 | 67.5 | 79.2 | 81.6 | 42 |
| 850 | 73.0 | 83.2 | 85.2 | 43 |
| 900 | 77.1 | 86.5 | 88.2 | 44 |
| 950 | 78.0 | 88.8 | 90.2 | 45 |
| 1000 | 83.8 | 90.8 | 92.0 | 46 |
| 1050 | 86.0 | 92.1 | 93.3 | 47 |
| 1100 | 87.2 | 92.9 | 94.0 | 48 |
| 1150 | 86.6 | 92.1 | 93.3 | 49 |
| 1200 | 85.2 | 91.8 | 92.9 | 50 |
| 450 | 0.7 | 2.5 | 4.0 | 52 |
| 500 | 5.0 | 14.2 | 18.2 | 56 |
| 550 | 15.0 | 30.0 | 34.8 | 57 |
| 600 | 26.8 | 44.0 | 48.1 | 59 |
| 650 | 38.8 | 56.0 | 60.2 | 60 |
| 700 | 49.0 | 65.7 | 69.1 | 61 |
| " * | 49.3 | 65.7 | 69.3 | 62 |
| 750 | 58.5 | 73.0 | 76.0 | 63 |
| 800 | 65.2 | 78.2 | 80.8 | 64 |
| 850 | 70.7 | 82.2 | 84.5 | 65 |
| 900 | 75.0 | 85.5 | 87.2 | 66 |
| 950 | 79.2 | 88.5 | 90.0 | 67 |
| 1000 | 82.7 | 90.8 | 92.0 | 68 |
| 1050 | 85.0 | 92.0 | 93.0 | 69 |
| 1080 | 85.7 | 92.2 | 93.2 | 70 |

| | | | | |
|------|------|------|------|----|
| 1100 | 95.3 | 94.2 | 87.0 | 56 |
| 1150 | 95.1 | 94.1 | 86.5 | 57 |
| 1200 | 94.9 | 93.8 | 86.0 | 58 |
| 450 | 8.3 | 8.0 | 4.2 | 59 |
| 500 | 28.0 | 27.0 | 17.2 | 60 |
| 550 | 45.0 | 43.6 | 30.8 | 61 |
| 600 | 58.5 | 56.5 | 42.0 | 62 |
| 650 | 69.0 | 67.0 | 52.0 | 63 |
| 700 | 76.0 | 74.0 | 60.0 | 64 |
| " * | 76.2 | 74.5 | 60.7 | 65 |
| 750 | 82.0 | 80.1 | 67.0 | 66 |
| 800 | 86.0 | 84.2 | 71.0 | 67 |
| 850 | 88.8 | 87.0 | 74.5 | 68 |
| 900 | 90.6 | 89.3 | 77.3 | 69 |
| 950 | 92.7 | 91.3 | 80.2 | 70 |
| 1000 | 94.0 | 92.8 | 82.6 | 71 |
| 1050 | 95.0 | 94.0 | 84.1 | 72 |
| 1100 | 95.3 | 94.2 | 84.9 | 74 |
| 1150 | 94.9 | 93.6 | 84.0 | 75 |
| 1200 | 94.9 | 93.5 | 84.0 | 76 |

Table 2b. Percentage transmittance of the mixed solutions

| D. A. H. CONC. | 1.56** (mM/L) | 6.25 " | 12.5 " | t (min.) |
|------------------------|---------------|--------|--------|----------|
| λ_0 (m μ) | | | | |
| 450 | 7.2 % | 3.5 % | 7.0 % | 23 |
| 500 | 25.8 | 16.9 | 24.5 | 24 |
| 550 | 42.2 | 32.0 | 41.0 | 25 |
| 600 | 55.8 | 45.6 | 54.2 | 26 |
| 650 | 66.3 | 57.1 | 65.1 | 27 |
| 700 | 73.8 | 66.2 | 73.0 | 28 |
| " * | 74.3 | 67.0 | 73.5 | 29 |
| 750 | 79.9 | 73.3 | 79.2 | 30 |
| 800 | 84.0 | 78.8 | 83.7 | 31 |
| 850 | 87.0 | 82.5 | 86.9 | 32 |
| 900 | 89.7 | 86.0 | 89.2 | 33 |
| 950 | 91.3 | 88.2 | 91.2 | 34 |
| 1000 | 93.0 | 90.1 | 92.7 | 35 |
| 1050 | 94.0 | 91.7 | 93.9 | 36 |
| 1100 | 94.2 | 92.0 | 94.0 | 37 |
| 1150 | 94.2 | 92.0 | 94.0 | 38 |
| 1200 | 94.0 | 91.9 | 93.9 | 39 |
| 450 | 6.9 | 3.2 | 6.7 | 40 |
| 500 | 24.7 | 15.8 | 23.5 | 41 |
| 550 | 41.3 | 31.0 | 40.2 | 42 |
| 600 | 54.5 | 44.2 | 53.5 | 43 |
| 650 | 65.7 | 56.3 | 64.9 | 44 |
| 700 | 73.0 | 65.5 | 72.6 | 45 |
| 750 | 79.5 | 73.0 | 79.2 | 47 |
| 800 | 83.7 | 78.0 | 83.3 | 48 |
| 850 | 87.0 | 82.2 | 86.9 | 49 |
| 900 | 89.2 | 85.7 | 89.2 | 50 |
| 950 | 91.8 | 88.6 | 91.8 | 51 |
| 1000 | 92.3 | 90.0 | 92.5 | 52 |
| 1050 | 93.9 | 91.5 | 93.9 | 53 |

| | | | | |
|------|------|------|------|----|
| 1100 | 85.8 | 92.2 | 93.1 | 71 |
| 1150 | 85.7 | 92.1 | 93.1 | 72 |
| 1200 | 84.3 | 91.5 | 92.5 | 73 |
| 450 | 1.2 | 2.7 | 4.0 | 75 |
| 500 | 5.0 | 14.0 | 17.5 | 76 |
| 550 | 14.0 | 29.0 | 33.2 | 77 |
| 600 | 25.0 | 42.5 | 47.0 | 78 |
| 650 | 36.4 | 54.8 | 59.0 | 79 |
| 700 | 47.0 | 64.7 | 68.0 | 80 |
| " * | 47.2 | 65.0 | 68.5 | 81 |
| 750 | 56.0 | 72.3 | 75.2 | 82 |
| 800 | 63.0 | 77.5 | 80.0 | 83 |
| 850 | 69.2 | 82.2 | 84.2 | 84 |
| 900 | 73.6 | 85.2 | 87.0 | 85 |
| 950 | 78.0 | 88.3 | 90.0 | 86 |
| 1000 | 81.0 | 90.0 | 91.3 | 87 |
| 1050 | 83.8 | 91.9 | 92.8 | 88 |
| 1100 | 85.0 | 92.0 | 93.1 | 90 |
| 1150 | 84.0 | 92.0 | 93.0 | 91 |
| 1200 | 83.3 | 91.2 | 92.2 | 92 |

Table 2b (continued)

| | | | | |
|------|------|------|------|----|
| 1100 | 94.1 | 92.0 | 94.1 | 54 |
| 1150 | 94.1 | 92.0 | 94.1 | 55 |
| 1200 | 93.9 | 91.6 | 93.9 | 56 |
| 450 | 6.2 | 3.0 | 6.1 | 57 |
| 500 | 23.5 | 15.0 | 22.9 | 58 |
| 550 | 40.0 | 30.0 | 39.6 | 59 |
| 600 | 54.0 | 43.6 | 53.0 | 60 |
| 650 | 64.5 | 55.2 | 64.0 | 61 |
| 700 | 73.2 | 65.5 | 73.0 | 62 |
| 750 | 78.9 | 72.0 | 78.7 | 63 |
| 800 | 83.1 | 77.1 | 83.0 | 64 |
| 850 | 86.6 | 82.0 | 86.7 | 65 |
| 900 | 89.0 | 85.0 | 89.1 | 66 |
| 950 | 91.0 | 88.0 | 91.0 | 67 |
| 1000 | 92.5 | 90.0 | 92.9 | 68 |
| 1050 | 93.3 | 91.0 | 93.5 | 69 |
| 1100 | 94.0 | 92.0 | 94.0 | 70 |
| 1150 | 93.9 | 91.8 | 93.9 | 71 |
| 1200 | 93.7 | 91.2 | 93.7 | 72 |
| 450 | 6.0 | 2.7 | 5.9 | 73 |
| 500 | 22.8 | 14.4 | 22.0 | 74 |
| 550 | 39.5 | 29.0 | 39.0 | 75 |
| 600 | 53.0 | 42.9 | 52.4 | 76 |
| 650 | 64.0 | 54.8 | 63.7 | 77 |
| 700 | 72.8 | 65.0 | 72.5 | 78 |
| 750 | 78.6 | 72.0 | 78.6 | 79 |
| 800 | 82.9 | 77.1 | 82.9 | 80 |
| 850 | 86.2 | 81.7 | 86.5 | 81 |
| 900 | 89.0 | 85.0 | 89.0 | 82 |
| 950 | 91.0 | 87.9 | 91.0 | 83 |

Measurement has been done with use of a Beckman type spectrophotometer, where the length of absorbing layer of solution is 1 cm.

* Exchange of photo-multiplier for Cs photo-tube.

** A different source of the sol has been used.

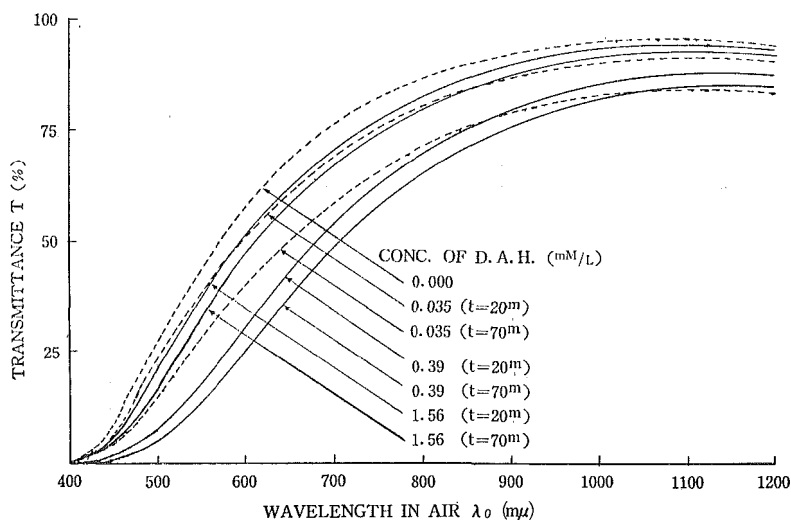


Fig. 3. Absorption curves of the mixed solutions.

This may be due to the adsorption of D.A.H. molecules by the colloid particles. Figure 3 shows the absorption curves of the mixed solutions at the certain time t elapsed after the mixing. The curves at the intersecting point are always steeper when the D.A.H. concentration is high than when it is low.

Absorption at the wavelength 422 mμ.

As shown in Fig. 4, an absorption band of AgI appears at the wavelength 422 mμ, and the minimum point of the transmittance shifts from 422 mμ to 428 mμ according to the increase of turbidity.

Such relation can be observed when the sol is diluted down to the concentration of 0.44 mM/L, whose coagulation and peptization values being found 0.08 mM/L and 0.35 mM/L, respectively.

Variation of the maximum transmittance.

The maximum point of the transmittance appears in the neighbourhood of wavelength 1100 mμ. The curves are less steep at this point and therefore the exact position of the maximum point is difficult to find.

Analysis of the transmission.

From the results obtained in Table 2, the turbidity τ can be determined, applying the following empirical formula.⁽⁶⁾

$$\tau = \frac{KR^{n-1}}{\lambda^n}, \quad (1)$$

where, R : radius of the particle.

λ : wavelength in solvent, namely, in water in this experiment.

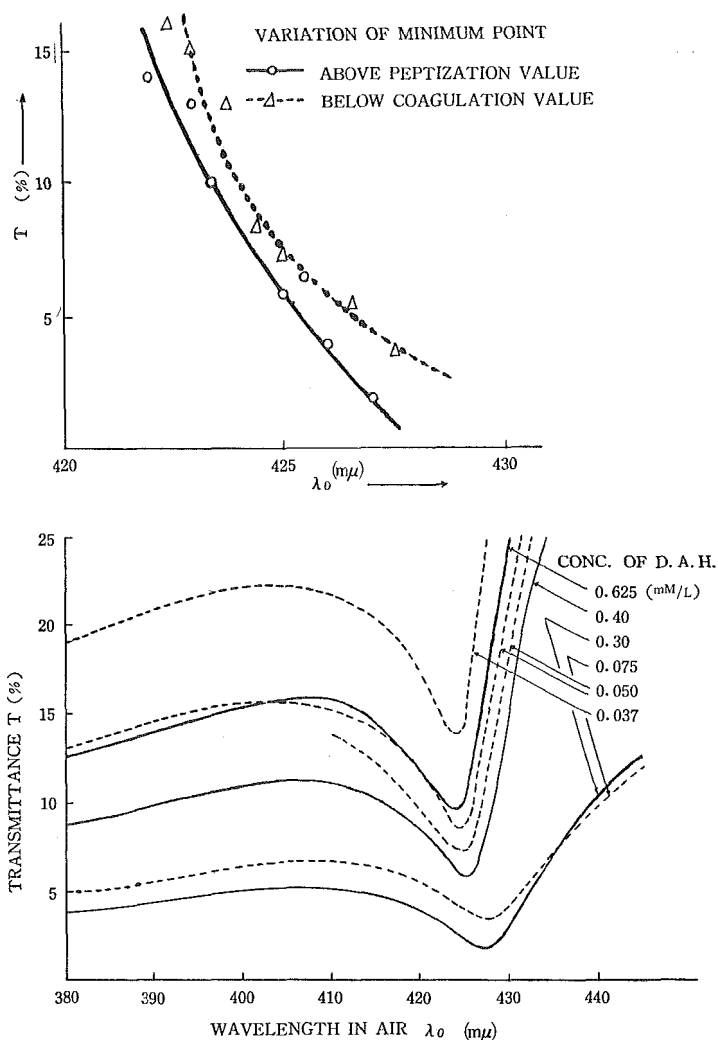


Fig. 4. Absorption at the wavelength 422~428 mμ.

K: proportional constant unrelated with R and λ .

From the graph of $\log \tau \sim \log \lambda$ or $\log \tau \sim \log \lambda_0$ (λ_0 represents the wavelength in air) the index of λ can be obtained as follows:

$$n = -\frac{d \log \tau}{d \log \lambda} = -\frac{d \log \tau}{d \log \lambda_0} \quad (2)$$

As shown in Fig. 5 and Table 3 the value of n varies from 4.0 to 2.7. When n is 4.0, the well-known formula of Rayleigh is applicable.⁽⁵⁾

$$\tau = \frac{24\pi^3 N V^2}{\lambda^4} \left(\frac{m^2 - 1}{m^2 + 2} \right)^2 \quad (3)$$

where, N: number of the particles in unit volume.

$m=n/n_0$, n : refractive index of the particle. n_0 : that of solvent.

In this case the radius R of the particle is smaller than 0.05λ . When R grows greater than 0.05λ , n becomes smaller than 4.0. These relations between n and R have been already reported by some researchers.⁽⁶⁾⁽⁷⁾

Table 3. Values of $\log \tau$ $[\tau]=[\text{cm}^{-1}]$

| D. A. H. CONC. (mM/l.) | | 0.000 | | 0.012 | | 0.035 | |
|---------------------------|-----------|----------------|-------------|------------------|-------------|-----------------|-------------|
| | | $t=0m$ $n=4.0$ | | $t=80m$ $n=3.75$ | | $t=70m$ $n=2.7$ | |
| | | T (%) | $\log \tau$ | T (%) | $\log \tau$ | T (%) | $\log \tau$ |
| λ_0 | λ | | | | | | |
| $m\mu$ | $m\mu$ | | | | | | |
| 650 | 489 | 69.4 | i. 5625 | 66.7 | i. 6074 | 51.1 | i. 8270 |
| 700 | 526 | 77.3 | .4107 | 74.1 | .4768 | 59.4 | .7167 |
| 750 | 565 | 82.7 | .2786 | 80.0 | .3486 | 66.3 | .6138 |
| 800 | 603 | 86.8 | .1510 | 84.1 | .2384 | 70.5 | .5438 |
| 850 | 641 | 89.5 | .0451 | 86.8 | .1509 | 74.1 | .4768 |
| 900 | 678 | 91.6 | .2.9431 | 89.2 | .0580 | 77.3 | .4107 |
| 950 | 714 | 93.2 | .8477 | 91.3 | .2.9592 | 80.2 | .3437 |
| 1000 | 751 | 94.5 | .7526 | 92.7 | .8797 | 82.8 | .2759 |

| D. A. H. CONC. (mM/l.) | | 0.39 | | | | 0.78 | |
|---------------------------|-----------|----------------|-------------|-----------------|-------------|----------------|-------------|
| | | $t=0m$ $n=4.0$ | | $t=80m$ $n=3.6$ | | $t=0m$ $n=4.0$ | |
| | | T (%) | $\log \tau$ | T (%) | $\log \tau$ | T (%) | $\log \tau$ |
| λ_0 | λ | | | | | | |
| $m\mu$ | $m\mu$ | | | | | | |
| 650 | 489 | 48.0 | i. 8657 | 36.3 | 0.0058 | 60.6 | i. 6997 |
| 700 | 526 | 58.2 | .7375 | 47.0 | i. 8780 | 69.6 | .5592 |
| 750 | 565 | 67.8 | .5896 | 56.3 | .7593 | 76.0 | .4385 |
| 800 | 603 | 72.9 | .4999 | 63.4 | .6587 | 81.1 | .3212 |
| 850 | 641 | 77.8 | .3997 | 69.6 | .5592 | 85.0 | .2109 |
| 900 | 678 | 81.8 | .3030 | 74.0 | .4787 | 88.0 | .1067 |
| 950 | 714 | 85.4 | .1982 | 78.3 | .3885 | 90.4 | .0040 |
| 1000 | 751 | 89.0 | .0665 | 81.5 | .3108 | 92.5 | .2.8919 |

| D. A. H. CONC. (mM/l.) | | 0.78 | | 1.56 | | | |
|---------------------------|-----------|-----------------|-------------|----------------|-------------|-----------------|-------------|
| | | $t=80m$ $n=4.0$ | | $t=0m$ $n=4.0$ | | $t=80m$ $n=4.0$ | |
| | | T (%) | $\log \tau$ | T (%) | $\log \tau$ | T (%) | $\log \tau$ |
| λ_0 | λ | | | | | | |
| $m\mu$ | $m\mu$ | | | | | | |
| 650 | 489 | 54.8 | i. 7792 | 64.6 | i. 6405 | 58.9 | i. 7237 |
| 700 | 526 | 64.8 | .6373 | 73.1 | .4960 | 68.2 | .5829 |
| 750 | 565 | 72.4 | .5092 | 79.2 | .3677 | 75.3 | .4529 |
| 800 | 603 | 77.6 | .4042 | 83.7 | .2502 | 80.2 | .3437 |
| 850 | 641 | 81.9 | .3003 | 87.0 | .1438 | 84.2 | .2355 |
| 900 | 678 | 85.2 | .2046 | 90.0 | .0227 | 87.0 | .1438 |
| 950 | 714 | 88.2 | .0989 | 92.0 | .2.9211 | 89.6 | .0407 |
| 1000 | 751 | 90.3 | .0087 | 94.0 | .7915 | 91.5 | .2.9486 |

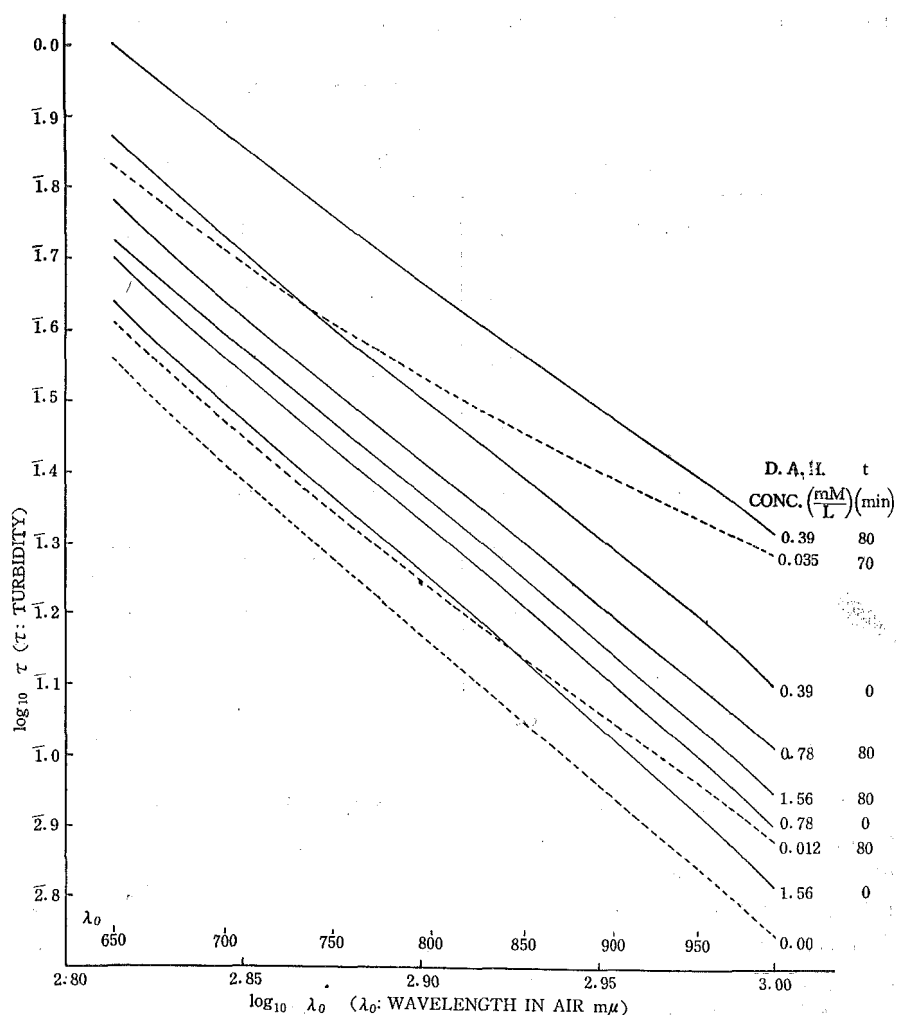


Fig. 5. Curves representing $\log \tau$ plotted against $\log \lambda_0$

Ratio of refractive index and radius of particle.

It is assumed that the increase of turbidity which takes place immediately after the mixing corresponds to the increase of m , the ratio of refractive index of the sol and its solvent, while the successive increase is due to the aggregation of particles.

In case of $n=4.0$, the radius of particle R and the ratio m can be obtained from Rayleigh's formula (3) as shown in Table 4, where, m , the ratio of refractive index of AgI in solvent (water), is equal to 1.7 and NV , the volume fraction of 2.2 mM/L AgI sol, is 9.1×10^{-5} . In the calculation of

R and m, the wavelength in water has been controlled to take a value between 603 $m\mu$ and 641 $m\mu$, where n is 4.00 in the original sol.

Table 4. Values of m, n and R.

| D. A. H. CONC. (mM/L.) | m | t (min) | n | R ($m\mu$) |
|---------------------------|-----|---------|-----|--------------|
| 0.000 | 1.7 | 40 | 4.0 | 34 |
| | | 80 | 4.0 | 35 |
| 0.012 | 1.7 | 40 | 3.8 | |
| | | 80 | 3.7 | |
| 0.035 | 1.7 | 40 | 3.2 | |
| | | 70 | 2.7 | |
| 0.39 | 2.3 | 40 | 3.8 | |
| | | 80 | 3.6 | |
| 0.78 | 1.9 | 40 | 4.0 | 35 |
| | | 80 | 4.0 | 36 |
| 1.56 | 1.8 | 40 | 4.0 | 35 |
| | | 80 | 4.0 | 36.5 |
| 6.25 | 2.0 | 40 | 4.0 | 35 |
| | | 80 | 4.0 | 36 |
| 12.5 | 1.8 | 40 | 4.0 | 34.5 |
| | | 80 | 4.0 | 35 |

"m" is one of the important factors which indicates the state of the surface of the particles. It takes the maximum value when the concentration of D. A. H. is 0.39 mM/L. On the other hand R is smaller at D. A. H. concentration of 0.78~12.5 mM/L and greater at 0.00~0.39 mM/L, according to the fact that the sol particles aggregate on losing their electric charge by the adsorption of the cationic agent.

Radius of the particle observed by electron microscope.

Fig. 6 shows the colloid particles observed by electron microscope without metallic shadow casting. The approximate values of the radii are shown in Table 5, although they vary slightly according to optical fields.

Table 5. R obtained from the electron micrograph.

| D. A. H. CONC. (mM/L.) | 0.000 | 0.035 | 0.78 | 1.56 | 12.5 |
|---------------------------|-------|-------|------|------|------|
| R ($m\mu$) | 13 | 13 | 16 | 17 | 19 |

Only separate particles of clear roundness are picked up as the objects of

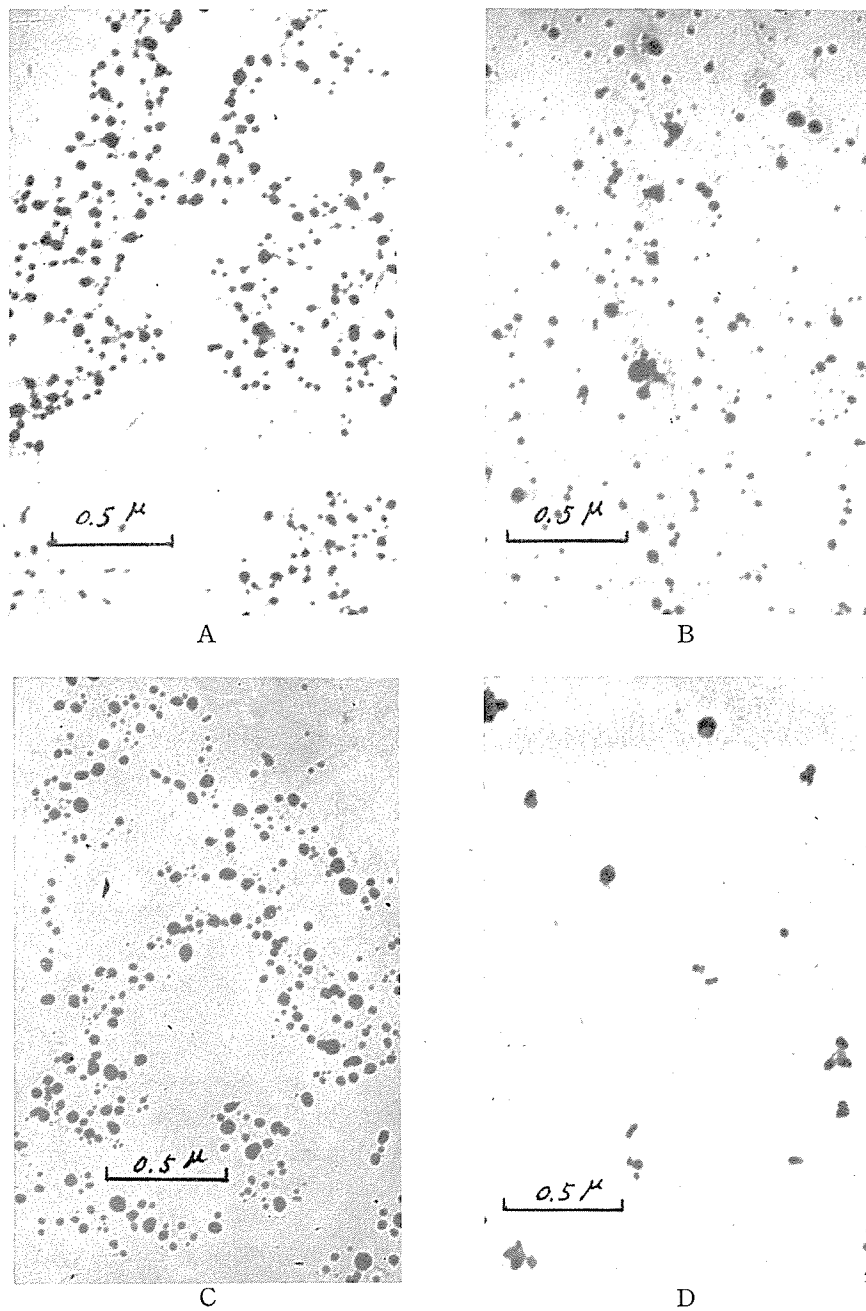


Fig. 6. Electron micrographs of AgI sol mixed by D.A.H. of varied concentrations. (A) 0.00mM/L, (B) 0.78mM/L, (C) 1.56mM/L, (D) 12.5mM/L.

observation, and those which have lost their round forms due to aggregation are excluded from observation, because it is rather difficult to determine whether they have lost their round forms in the solutions or have overlapped themselves while they were dried on the collodion membrane. The radii of the original sol particles are less than the half of those obtained from the transmittance and the particles grow larger and larger with the increase of the concentration of the agent added.

This is contrary to what was observed in Table 4.

The above fact shows that the individual and separate particles are slightly larger and more stable and less inclined to aggregate when the concentration of D. A. H. is above 0.78 mM/L than those when the concentration is under 0.39 mM/L .

Mechanism of the coagulation and peptization.

In their reports^{(3) (4)} on the mechanism of coagulation and peptization of colloid particles by surface active agents, K. Meguro and S. Saito assumed that the particles, once losing their electric charge due to the adsorption of the agent molecules with opposite charge, become hydrophobic and coagulate, but they gain the electric charge again and become hydrophilic when the surface active agent is added further.

The present author is inclined to think that the particle must be the most hydrophobic when the ratio m is the largest and consequently that the main cause of coagulation, when the concentration of D. A. H. is not greater than its coagulation value 0.08 mM/L , should be the neutralization of the electric charge.

Light scattering by large particles.

When the radius of the particle of sol is larger than 0.05λ , Rayleigh's formula (3) is not applicable, and n , index of λ , will take smaller values than 4.0. In the present author's experiment, R , the radius of the particle, can not be obtained from the empirical formula (1). But another formula

$$\frac{1}{\tau\lambda^2} = \frac{K}{R^2}\lambda + \frac{K'}{R^4} \quad (4)$$

(NV=constant)

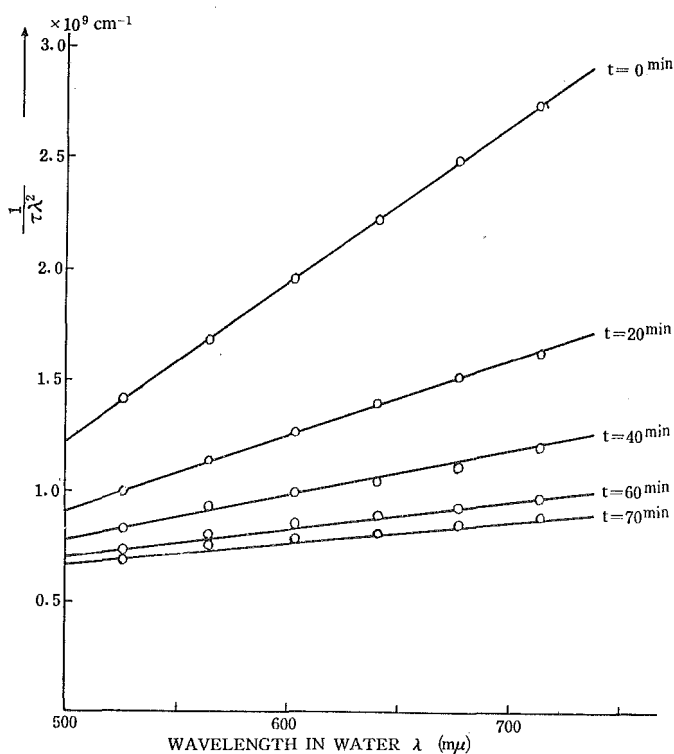
is satisfactorily applied and, moreover, the radius R calculated from this formula agrees with Heller's n - R relation⁽⁷⁾ obtained with polystyrene or polyisoprene emulsion. (Fig. 7.)

Table 6 shows the values of R calculated by this formula, when D. A. H. concentration is 0.035 mM/L .

Table 6. Relation between n and R .

| TIME t (min.) | n | R ($m\mu$) |
|-----------------|-----|----------------|
| 0 | 4.0 | 34 |
| 20 | 3.6 | 51 |
| 40 | 3.2 | 68 |
| 60 | 2.8 | 80 |
| 70 | 2.7 | 88 |

There is a tendency of diminishing in the first term of the right side of the equation (4) according to the time elapsed, during which the particles grow larger as shown in Fig. 7.

Fig. 7. $1/\tau\lambda^2 \sim \lambda$ (D. A. H. 0.035 mM/L)

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