

1 High-speed synthesis of thermo-responsive
2 polymers by boosted polymerization of *N,N*-
3 diethyl acrylamide in high-temperature water

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13

14 Abstract

15 The transition toward a circular plastic economy and sustainable chemical industries requires
16 the development and implementation of green methods of free-radical polymerization. In this
17 study, the high-speed radical polymerization of *N,N*-diethyl acrylamide (DEAA) was
18 achieved in high-temperature water (150 °C, 0.5 MPa) without using potentially
19 contaminating organic solvents. Precipitation polymerization was completed within 2 min.
20 The molecular weight of the resulting polymer (27.7×10^3 ; dispersity of 1.78) was
21 comparable to that of polymers obtained by typical polymerization at 70 °C and significantly
22 exceeding those of polymers obtained by polymerization in high-temperature organic
23 solvents. This implies that the main factor governing the polymerization rate is a kinetic
24 effect due to hydrogen bonding between the carbonyl groups and water molecules; under
25 these conditions, disproportionation termination was suppressed. The polymerization process
26 developed herein using high-temperature water is offers the benefits of a short reaction time
27 and low environmental impact, thus holding great promise for industrial applications.

28 Keywords: Environment-friendly polymerization, Radical polymerization, High production
29 rate, Molecular weight, Dispersity, Solvent-free, Recombination.

30

31 INTRODUCTION

32 The increasing awareness regarding global warming and related environmental issues is
33 changing our view on production processes in terms of, not only cost and efficiency, but also
34 environmental impact in view of achieving a sustainable society.^{1,2} The polymeric materials
35 widely exploited as plastic, fibers, rubbers, and adhesives are invaluable to society. Since the
36 discovery of chloroprene polymerization,³ the radical polymerization of vinyl monomers,
37 such as styrene, (meth)acrylates, vinyl acetate, and acrylamides, has significantly contributed
38 to industrial polymer production. In radical polymerization, processing temperature
39 substantially affects polymer formation kinetics, final molecular weight (MW), and MW
40 dispersity.⁴ Therefore, temperature control is crucial for obtaining the desired products.
41 Given that bulk polymerization is exothermic and therefore suffers from excessive heat
42 release, industrial-scale radical polymerization typically involves the suspension
43 polymerization of hydrophobic vinyl monomers in water and solution-phase polymerization
44 in homogeneous systems. To avoid the unfavorable use of organic solvents, supercritical
45 fluids^{5,6} and high-temperature water (*i.e.*, water at 100–374 °C and 0.1–22.1 MPa with
46 controllable dielectric constant and ionic product^{7–10}) are used in solution polymerization. For

47 example, Kinoshita *et al.*¹¹ conducted the radical polymerization of acrylic acid in high-
48 temperature water using a flow-type apparatus. Typically, radical polymerization is
49 performed around the 10-h half-life temperature (T_{10}) of the initiator to avoid frequent
50 termination and MW decrease. Nevertheless, the radical polymerization of acrylic acid in
51 high-temperature water generates high-MW polymers within several minutes.¹¹

52 Although radical polymerization in high-temperature water may contribute to improved
53 polymer production and thus promote the establishment of a sustainable society, the use of
54 flow-type reactors in radical polymerization limits the range of applicable monomers,¹²
55 because both the monomers and resulting polymers must be soluble in water to keep the
56 reaction system homogeneous. In particular, *N,N*-diethyl acrylamide (DEAA) is soluble in
57 water, whereas the corresponding polymer is insoluble above the lower critical separation
58 temperature (LCST) of 32 °C.¹³ Therefore, DEAA is not a suitable monomer for flow-type
59 reactors. In this study, the radical polymerization of DEAA was performed in high-
60 temperature water and other solvent in a batch-type reactor under tunable reaction (e.g.
61 reaction time and temperature). The behavior and mechanism of the polymerization process
62 in high-temperature water were investigated.

63

64 MATERIALS AND METHODS

65 DEAA was kindly donated by KJ Chemicals Co. The initiator [4,4'-azobis(4-cyanovaleric
66 acid), V-501], ethanol (EtOH), and *N,N*-dimethylacetamide (DMAc) were purchased from
67 FUJIFILM Wako Pure Chemical Corporation. D₂O (100.0 at% D) was supplied from Acros
68 Organics. 1,4-Dioxane (DO) was purchased from Kishida Chemical Co., and *N,N*-
69 dimethylformamide (DMF) was purchased from Yoneyama Yakuhin Kogyo Co., Ltd.

70 Gas chromatography (GC) was performed using a Shimadzu GC-2014 gas chromatograph
71 equipped with a flame ionization detector (FID) and an SH-Rtx-5 capillary column (30 m ×
72 0.32 mm, 0.25 μm; Restek) with He as the carrier gas (linear velocity = 30 cm s⁻¹) and make-
73 up gas. The vaporization chamber was maintained at the starting temperature of 50 °C for 2
74 min and subsequently heated to 300 °C at a rate of 20 °C min⁻¹.

75 MWs and their distributions were determined using size-exclusion chromatography (SEC),
76 which was performed using a JASCO EXTREMA chromatograph equipped with two SEC
77 columns (Shodex HK-404L) and ultraviolet (UV-4070, JASCO, 235 nm) and refractive
78 index (RI-4035, JASCO) detectors. Tetrahydrofuran (Wako Pure Chemical Industries, HPLC

79 grade, flow rate = 0.4 mL min⁻¹) was used as the eluent at 40 °C. MWs were calibrated using
80 standard polystyrene samples (TSK-gel oligomer kit, Tosoh, MW = 1.03 × 10⁶, 3.89 × 10⁵,
81 1.82 × 10⁵, 3.68 × 10⁴, 1.36 × 10⁴, 5.32 × 10³, 3.03 × 10³, and 8.73 × 10²).

82 A 6-mL stainless-steel tube was charged with a solution of DEAA (0.200 g, 1.57 mmol)
83 and V-501 (5 mg, 17.8 μmol) in H₂O (3.0 g), immersed into an oil bath held at 150 °C for a
84 predetermined time (2–180 min), and rapidly cooled to 20–25 °C in a cold-water bath. The
85 temperature inside the tube was directly measured using a thermocouple. An analogous
86 procedure was adopted for polymerization at 70 °C, and in other solvents, and in the bulk.

87 Monomer conversion was determined from the GC-FID peak areas of DEAA before and
88 after polymerization as

$$89 \quad \text{Monomer conversion (\%)} = \left(1 - \frac{\text{DEAA peak area after polymerization}}{\text{DEAA peak area before polymerization}}\right) \times 100. \quad (1)$$

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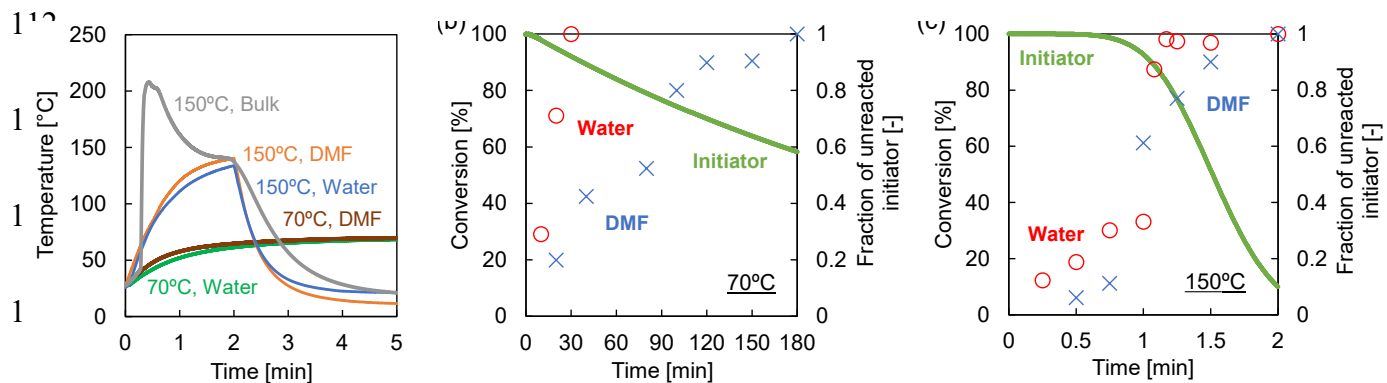
91 RESULTS AND DISCUSSION

92 The heating process affecting radical polymerization⁴ was investigated in a batch-type
93 stainless-steel reaction tube. Figure 1 (a) shows the internal temperature profiles of the batch
94 reactor immersed into oil baths heated to different temperature. Given that the reaction started

95 when the reactor was submerged into the oil bath, the reaction time included the initial
96 heating period. After a given reaction time, the reactor was removed from the oil bath and
97 was rapidly quenched in a cold-water bath to cool it to 20–25 °C. The reaction was also
98 performed without any solvents (bulk polymerization).

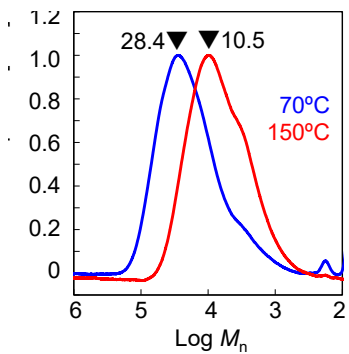
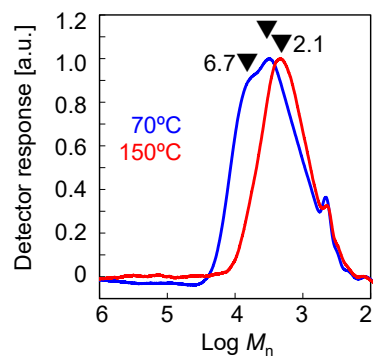
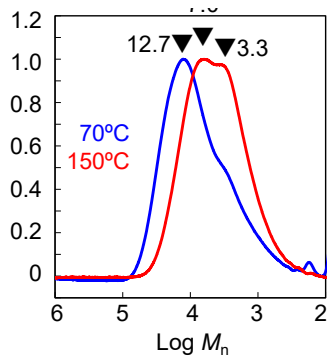
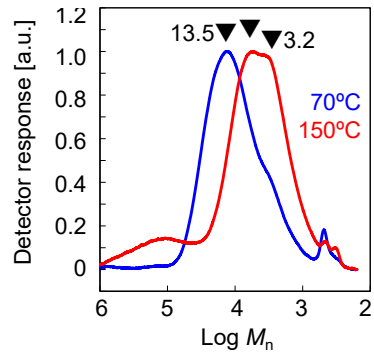
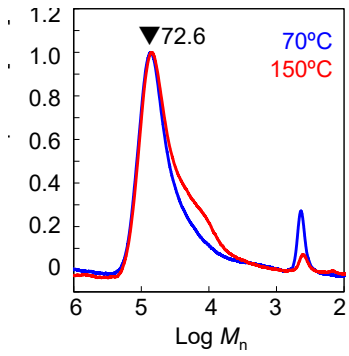
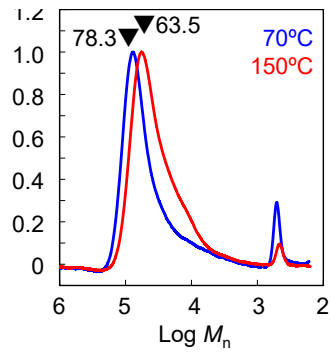
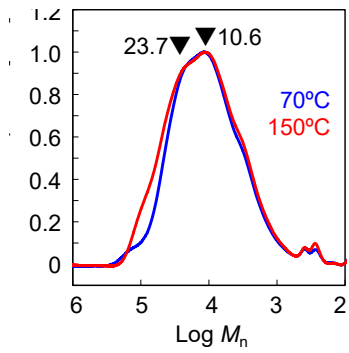
99 At 70 °C, the heating period (2 min) was much shorter than the reaction time (180 min),
100 thus exerting a modest influence. Conversely, at 150 °C (reaction time 2 min), polymerization
101 occurred within the heating period, which critically affected the obtained products. Owing to
102 the high heat capacity of the stainless-steel reactor, the heating processes at 70 and 150 °C
103 were similar, although the molar heat capacities of water¹⁴ and DMF¹⁵ at a constant pressure
104 were different, 75.3 and 146 J K⁻¹ mol⁻¹, respectively. For bulk polymerization, no solvent
105 was available to dissipate the heat of polymerization, and the temperature rapidly exceeded
106 the set value (150 °C) because of the autoacceleration of exothermic propagation.¹⁶
107 Afterwards, the temperature gradually decreased because of the deceleration of the
108 polymerization reaction due to an increase in viscosity.¹⁷ Therefore, the outcomes of bulk
109 polymerization tests were not influenced by the set temperature, with polymerizations at 70
110 and 150 °C resulting in similar MW distributions (Figure 2 (a) and Table S1).

111



116

117 **Figure 1.** (a) Internal temperature profiles of the reactor over time. (b, c) Correlation between
118 DEAA conversion and reaction time in water and DMF at (b) 70 °C and (c) 150 °C; and
119 calculated degree of the thermal homolytic cleavage of the initiator.



121 **Figure 2.** Molecular weight distributions of polymers obtained in (a) bulk, (b) water, (c)
122 deuterated water, (d) *N,N*-dimethylformamide, (e) *N,N*-dimethylacetamide, (f) ethanol, and
123 (g) 1,4-dioxane at 70 and 150 °C.

124

125 Figures 1 (b) and (c) show the reaction-time-dependent conversions of DEAA in water (red
126 circles) and DMF (blue crosses) at the set temperatures of 70 °C and 150 °C, respectively.
127 At 70 °C, the monomer conversion reached 100% after 30 min in water and after 180 min in
128 DMF. In contrast, complete monomer consumption at 150 °C in water and DMF were
129 achieved after 1.1 and 1.5 min, respectively. The average MWs and their dispersity in water
130 and DMF at 150 °C were almost constant regardless of monomer conversion (Table 1), which
131 indicated that the steady-state approximation was also valid under boosted polymerization
132 conditions. Therefore, the accelerated polymerization at 150 °C essentially followed the same
133 mechanism as the general radical polymerization at 70 °C. Nevertheless, when
134 polymerization at 150 °C performed in a transparent glass tube, we observed the precipitation
135 of the resulting polymer, poly(DEAA), in line with its insolubility in water above 32 °C
136 (Movie S1). Therefore, for lab-scale poly(DEAA) synthesis, batch-type reactors are preferred

137 to flow reactors. However, flow reactors would be promising for poly(DEAA) production at
138 an industrial scale.

139

140 **Table 1.** Monomer conversions and molecular weights obtained at different reaction times
141 in radical polymerization at 150 °C.

Solvent	Reaction time (min)	Monomer conversion (%)	$M_n (\times 10^{-3})$	$M_w (\times 10^{-3})$	\bar{D}
Water	0.75	30.1	21.4	28.9	1.35
Water	1	33.2	26.8	49.8	1.86
Water	1.08	87.4	21.0	30.9	1.47
Water	2	100	27.7	49.1	1.78
DMF	1.25	77.1	4.6	9.0	1.95
DMF	2	100	3.5	6.6	1.86

142

143 The green curves shown in Figures 1 (b) and (c) indicate the thermal cleavage degree of
144 the V-501 initiator at 70 and 150 °C, respectively, estimated by Equation (2):

145
$$k_d (s^{-1}) = 6.21 \times 10^{15} \exp\left(\frac{-1.33 \times 10^5}{RT}\right), \quad (2)$$

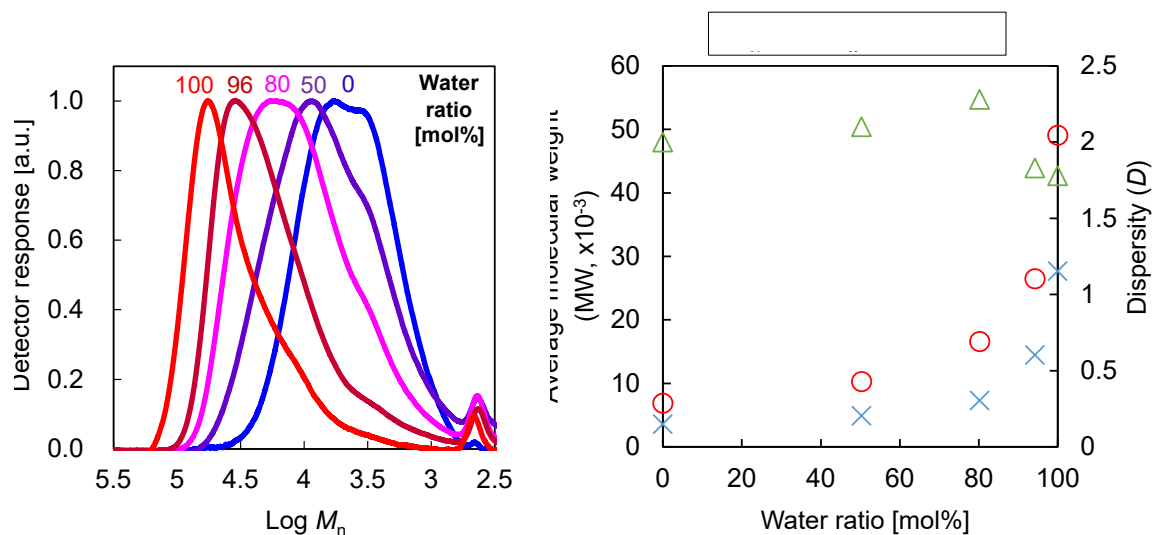
146 where k_d is the rate constant of thermal hemolytic cleavage, R is the universal gas constant,
147 and T is the absolute temperature. The activation energy and pre-exponential coefficient in
148 Equation (2) were measured in the temperature range of 40–80 °C¹⁸ and were assumed to be
149 independent of temperature, solvent type, and the monomer presence. At 70 °C, more than
150 half of the initiator was present even after 180 min. Conversely, at 150 °C, V-501 was almost
151 completely converted into radicals within 2 min. Therefore, the fast consumption of DEAA
152 at 150 °C was ascribed to the combined effects of fast propagation and sufficient radical
153 supply. Concurrently, high radical concentrations typically afford low-MW products because
154 they result in fast termination reactions and decreased monomer-to-radical ratios. When
155 organic solvents (DMF, DMAc, EtOH, and DO) were used, the MWs of products generated
156 at 150 °C were lower than those of products obtained at 70 °C (Figures 2 (d)–(g)). In contrast,
157 in water (H₂O and D₂O; Figures 2 (b) and (c), respectively), polymers with higher MWs were
158 obtained even at 150 °C, although the values were slightly lower than those for
159 polymerization at 70 °C. Therefore, in water, the high propagation rate was the main
160 contributor to the increased termination rate at high temperatures. The fact that polymers
161 obtained at 70 °C in water had higher MWs than those produced in organic solvents indicated

162 specific fast propagation. Water molecules formed hydrogen bonds with carbonyl groups,
163 resulting in fast DEAA polymerization, as previously reported for the polymerization of acryl
164 monomers.^{19–22} The difference between the MWs of products obtained at 70 and 150 °C was
165 smaller in D₂O than for water, which was ascribed to the higher strength and temperature
166 stability of deuterium bonds compared to hydrogen bonds.²³

167 Termination reactions in radical polymerization proceed via disproportionation and
168 recombination, with the latter mechanism affording products with double the MWs than those
169 achieved by the former. The unimodal MW distributions of products obtained at 70 °C
170 (Figure 2, blue lines) featured a main peak with a shoulder in the low-MW region, except for
171 polymerization in the bulk and in EtOH (Figures 2 (a) and (f), respectively). The main and
172 shoulder peaks resulted from recombination and disproportionation, respectively. Therefore,
173 recombination was the main termination pathway at 70 °C. Furthermore, the curves related
174 to polymerization in DMF, DMAc, and DO (red lines in Figures 2 (d), (e), and (g),
175 respectively) indicated that a bimodal distribution was obtained at 150 °C. The MW
176 corresponding to the first peak was twice that corresponding to the second peak, which
177 indicated that the first and second peaks corresponded to termination by recombination and

178 disproportionation, respectively. Conversely, the MW of the product formed in EtOH at 70
179 and 150 °C had a bi- and unimodal distribution, respectively, and was lower than those of
180 polymers formed in other solvents, which suggested that EtOH exerts a unique solvent effect.
181 In contrast to polymerization in organic solvents, the differences between the products
182 formed at 70 and 150 °C in water were negligible, and recombination was dominant at both
183 temperatures. These results highlight the solvent effect exerted via hydrogen bonding, which
184 promoted the propagation reaction, even at 150 °C. Thus, the specificity of water was crucial
185 for enhancing the polymerization reaction.

186



187

188 **Figure 3.** Effect of the water/DMF ratio on the (a) molecular weight distribution and (b)
189 average molecular weights and their dispersity (D) at 150 °C.

190

191 To assess the water volume required to promote high-speed polymerization, we conducted
192 polymerization experiments in water–DMF mixtures of different compositions and examined
193 the effects of solvent composition on MW distribution, average MW, and MW dispersity at
194 150 °C (Figure 3). The shape of the MW distribution changed from unimodal to bimodal
195 with increasing DMF content (Figure 3 (a)), in accordance with the change of the termination
196 mechanism discussed above. These results also suggest that in water, hydrogen bonding leads
197 to high-speed polymerization at high temperatures, affording high-MW products and
198 suppressing disproportionation termination. The MW of the polymer obtained at a DMF
199 content of 4 mol% was substantially lower than that obtained in pure water (Figure 3 (b)).
200 Therefore, a small amount of DMF was sufficient to affect polymerization behavior.

201 The polymerization solvent may also affect the mechanism of chain transfer to the polymer.
202 In water, when the monomer is soluble and the polymer is insoluble, precipitation
203 polymerization would occur. On the other hand, in organic solvents, the polymer may

204 dissolve without precipitating. Thus, chain transfer to the polymer in water could have been
205 suppressed by precipitation. If such chain transfer occurred in organic solvents, a branched
206 polymer with a multimodal and broad MW distribution should be formed. However, bimodal
207 and not multimodal MW distributions were obtained in organic solvents. Therefore, we
208 believe that chain transfer to the polymer did not occur in either water or organic solvents.

209 Considering non-isothermal polymerization (Fig. 1), the reactor temperature profile
210 obtained in water was almost identical to that obtained in DMF. If the bimodal MW
211 distributions in DMF were due to non-isothermal polymerization, the bimodal peaks should
212 have also been obtained in water. Therefore, non-isothermal polymerization was not the main
213 cause of the solvent effect on MW distributions.

214 A previous study of the radical polymerization of acrylamides at around the T_{10} of the
215 initiator²⁴ showed that each polymerization stage (initiation, propagation, and termination)
216 was affected by solvent type, which was attributed to various reasons, including chain
217 transfer to the solvent and differences in solvent polarity and dielectric constant. In addition,
218 the radical polymerization of acrylamides in water was significantly faster than that in other
219 organic solvents, and a higher polymerization rate and MW were observed when water was

220 added to dimethyl sulfoxide. Herein, we found that the effect of the solvent type at a high
221 temperature of 150 °C was similar to that at 70 °C. The higher polymerization rate and MW
222 observed for high-temperature water compared to those observed for organic solvents were
223 attributed to differences in propagation rate and termination mode, which are influenced by
224 the solvent polarity and dielectric constant.

225

226 CONCLUSIONS

227 High-temperature water (150 °C, 0.5 MPa) enabled the high-speed radical polymerization
228 of DEAA, resulting in complete conversion into high-MW products within a short time (2
229 min). Although the polymers obtained in water precipitated because of their low LCST, pure
230 water was more favorable than organic solvents, which induced disproportionation and
231 frequent termination reactions, even when added in small amounts as cosolvents. Further
232 work is required to elucidate the effect of polymer precipitation in various solvents at high
233 temperatures. A batch-type reactor was effective for application in such precipitation
234 polymerization reactions in water. However, given that a short reaction time (within 2 min)
235 was sufficient in high-temperature water, flow reactors may potentially be used in industrial

236 settings. High-speed radical polymerization offers the advantage of low environmental
237 impact and is completed in a short time without the use of any organic solvents. Moreover,
238 the examined process is promising for application in the polymer industry for reducing its
239 environmental impact and operating costs by considerably increasing the production rate.

240

241 ASSOCIATED CONTENT

242 **Supporting Information.** Details of the experimental conditions, monomer conversion,
243 and molecular weights and their distributions obtained at different temperatures (Table S1);
244 video showing the polymerization of DEAA in high-temperature water at 150 °C in a
245 transparent glass tube (Movie S1).

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249 **Author Contributions**

250 The manuscript was written through contributions of all authors. All authors have given
251 approval to the final version of the manuscript.

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254 substantial intellectual contributions to the conception of the project.

255 ABBREVIATIONS

256 DEAA, *N,N*-diethylacrylamide; DMAc, *N,N*-dimethylacetamide; DMF, *N,N*-
257 dimethylformamide; DO, 1,4-dioxane; EtOH, ethanol; FID, flame ionization detector; GC,
258 gas chromatography; LCST, lower critical separation temperature; MW, molecular weight.

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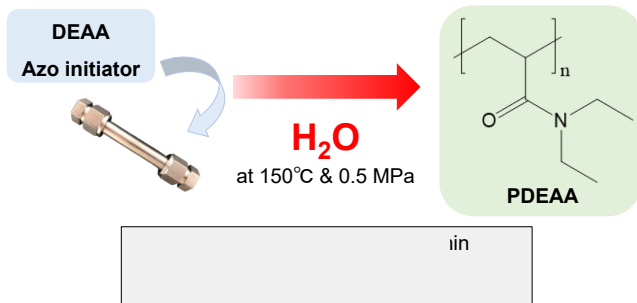
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326 Graphical Abstract



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